Methods for Pressurized Seal Systems

What are the best practices for ensuring the reliability of API Piping Plan 53C?

By Mark Savage
FSA Member, John Crane

There are many methods to pressurize the barrier fluid for a dual pressurized mechanical seal. Each method, or piping plan, uses a different mechanism to apply the pressure to the barrier fluid and, as a result, each has its own set of advantages.

One of these methods is American Petroleum Institute (API) Plan 53C. Although not as widely installed as a traditional API Plan 53A system, it does differentiate itself from other methods. API Plan 53C has the ability to change the barrier pressure as the pressure inside the pump changes.

This pressure tracking ability makes this system ideally suited to high-pressure pumps, or for pumps that tend to experience a wide range of operating pressures.

A Plan 53C barrier system consists of two main elements:

- **Barrier fluid circulating loop:** A pumping device within the mechanical seal circulates barrier fluid to a heat exchanger, where heat absorbed into the barrier fluid is dissipated and then the fluid is returned to the mechanical seal.

- **Piston accumulator:** Stores barrier fluid and amplifies pressure from the pump to pressurize the barrier fluid circulating loop.

The piston accumulator pressurizes the barrier fluid loop by using a reference pressure line connected to the pump. This reference line is used to pressurize one side of the piston, which pushes the piston against the barrier fluid located on the other side.

As the piston rod reduces the effective area of the piston face in contact with the barrier fluid, the barrier fluid pressure is amplified.

The pressure amplification ratio is simply the ratio of the area of each side of the piston.

The pressure amplification ratio can be calculated as:

\[
\text{ratio} = \frac{\text{area 1}}{\text{area 2}}
\]

Increasing the piston rod diameter has the effect of reducing Area 2, and thus increases the pressure amplification ratio.

Due to the practicalities of design and function, amplification ratios are typically in the range of 1.05 to 1.30.

---

Pressure ratios above this have large diameter piston rods (relative to the cylinder) and become longer in order to provide sufficient barrier fluid storage volume.

**Tracking the Barrier Pressure**

As the pressure changes in the reference line, the pressure produced by the piston accumulator and delivered to the barrier fluid circulating loop will change proportionally to the amplification ratio.

\[
\text{barrier pressure} = \text{reference pressure} \times \text{amplification ratio}
\]

The ability to track barrier pressure with respect to the reference pressure is what makes an API Plan 53C different from other dual seal barrier systems. Since the barrier pressure is generated by amplifying the reference pressure from the pump, the piston accumulator requires no external utilities to function, which further simplifies the installation and operation of a Plan 53C system.

**Pump Reference Pressure & Amplification Ratio Selection**

Selecting the right amplification ratio and reference pressure point on the pump pressure casing is key to ensuring the correct barrier pressure for the mechanical seal.

API 682 recommends a minimum barrier pressure of 1.4 bar/20 pounds.
per square inch (psi) above the seal chamber. The reference pressure and the amplification ratio need to be selected to meet this minimum requirement. Additionally, the range of pressure at the reference point must also be factored into the selection process.

For high pressure pumps, the seal chamber can be used as a reference pressure and meet the minimum differential pressure requirements. A simple connection in the seal chamber or mechanical seal gland plate can be used to plumb a reference line to the piston accumulator.

However, for low pressure pumps, a pressure higher than the seal chamber must be maintained in order to meet the minimum differential pressure requirements. Depending on the pump design, this can be the pump’s final discharge pressure or the discharge of an intermediate stage (if the pump is a multistage design).

An alternative design would be a piston accumulator with a “helper spring” that provides a minimum pressure offset.

**Installation & Commissioning**

The two elements of the Plan 53C system, the barrier fluid circulating loop (with heat exchanger) as well as the piston accumulator, need to address different factors.

The barrier fluid circulating loop needs to be installed to offer the least resistance to barrier fluid flow produced by the pumping ring located within the mechanical seal.

The location of the heat exchanger and the path of the interconnecting tubing between the heat exchanger and mechanical seal are critical to meeting this requirement. Additionally, provisions to vent the circulating loop must be incorporated so any trapped air can be removed from the system prior to commissioning.

A low point drain is also recommended when operators are decommissioning the system for maintenance.
The location of the piston accumulator is more flexible. The only flow that occurs in the piston accumulator is the slow movement of barrier fluid to replace any leakage that occurs from the mechanical seal.

When done correctly, the piston accumulator should be mounted in the vertical orientation (to assist with venting) with the piston rod protruding from the top of the accumulator.

A location accessible by maintenance personnel should be selected where the interconnecting piping does not obstruct maintenance access to the pump. A high point vent to remove air from the system and a connection to enable replenishment of barrier fluid must also be included.

**Piston Accumulator Operation**

During operation, barrier fluid is consumed due to normal leakage of the mechanical seal. Barrier fluid stored in the piston accumulator moves into the barrier fluid circulating loop to replace the lost barrier fluid, resulting in the piston and piston rod slowly moving upwards. The extension of the piston rod from the top of the accumulator provides a direct indication of the volume of barrier fluid remaining in the accumulator.

A scale can be mounted to a bracket adjacent to the piston rod to provide a local display of the remaining barrier fluid. Proximity switches can also be fitted at desired alarm points to provide a remote indication that minimum volume threshold points have been exceeded, or a linear position transmitter can be installed to provide a precise remote indication of the barrier fluid remaining.

A shield is recommended to prevent accidental damage and the effects of dirt and debris from weathering to the surface of the piston rod and piston rod seal.

Periodically, the consumed barrier fluid will need to be replenished. This is achieved by pumping barrier fluid from a reservoir into the piston accumulator. Typically, a wheeled cart with a small reservoir and pneumatic or hand pump is used to replenish the barrier fluid.

The replenishment interval is determined by the size of the piston accumulator and the rate of normal barrier fluid consumption of the mechanical seal.

**Plan 53C Limitation**

The pumped media is used as the source of pressure in the piston accumulator. So, the properties of this pumped fluid must be considered when selecting a Plan 53C system.

The following pumped fluids should be avoided to ensure reliable operation of the barrier system:

- **Pumped fluids that solidify at ambient conditions.** As there is effectively minimal flow of fluid in the reference line, the fluid in this line will, over time, cool down to ambient temperatures. Fluids that solidify as they cool can plug the...
reference line preventing the pump pressure from acting against the piston in the accumulator and resulting in loss of barrier pressure.

- **Pumped fluids that contain suspended solids.** The suspended solids can migrate into the piston accumulator and interfere with the function of the piston seal, causing wear and damage to the internal surfaces of the cylinder resulting in leakage past the piston seal and loss of barrier fluid.

- **Pumped fluids at elevated temperatures.** As the pumped fluid is introduced into the piston accumulator during commissioning, thermal damage to the piston seal can occur if it is exposed to temperatures above the limits of piston seal material(s).

- **Pumped fluids that are corrosive.** The compatibility of the materials of construction of the piston accumulator with the pumped fluid should be reviewed to ensure no corrosive damage occurs to the internal walls of the accumulator and to the piston seals.

**Conclusion**
Plan 53C pressurized seal systems offer the ability to adjust the barrier pressure as the pressure in the pump changes making this a simple, safe and reliable solution in a range of pumping applications.

The correct sizing of the piston accumulator, heat exchanger and barrier fluid flow rate together with best installation and operational practices are the key to years of reliable performance from a Plan 53C system.

**Next Month:**
What to know about expansion joints reducers

We invite your suggestions for article topics as well as questions on sealing issues so we can better respond to the needs of the industry. Please direct your suggestions and questions to sealingsensequestions@fluidsealing.com.

**Mark Savage** is a product group manager at John Crane, responsible for the design, development and application of metal bellows seals for pumps, compressors and rotating machinery. He has worked in the sealing industry for 25 years and has been involved with development of best practices for shaft seals and their support systems. Savage holds a Bachelor of Engineering from the University of Sydney, Australia. For more information, visit johncrane.com.